## **An Introduction to Charged Particles Tracking**

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#### **Contents**



### **Introduction**



### **Motion in Magnetic Field**

**In a magnetic field the motion of a charged particle is determined by the Lorentz Force**

$$
\left| \frac{d\mathbf{p}}{dt} = e \mathbf{v} \times \mathbf{B} \right|
$$

**Since magnetic forces do not change the energy of the particle**

$$
m_o \gamma \frac{d\mathbf{v}}{dt} = e \mathbf{v} \times \mathbf{B}
$$

$$
m_o \gamma \frac{d^2 \mathbf{r}}{dt^2} = e \frac{d \mathbf{r}}{dt} \times \mathbf{B}
$$

**using the path length** *<sup>s</sup>* **along the track instead of the time** *t*

$$
ds = vdt
$$

**we have**

$$
m_o \gamma v \frac{d^2 \mathbf{r}}{ds^2} = e \frac{d \mathbf{r}}{ds} \times \mathbf{B}
$$

**and finally**

$$
\frac{d^2\mathbf{r}}{ds^2} = \frac{e}{p}\frac{d\mathbf{r}}{ds} \times \mathbf{B}
$$

**In case of inhomogeneus magnetic field, B(s) varies along the track and to find the trajectory r(s) one has to solve a differential equation**

**In case of homogeneus magnetic field the trajectory is given by an helix**



### **Magnetic Spectrometers**

**Almost all High Energy experiments done at accelerators have a magnetic spectrometer to measure the momentum of charged particles**

**2 main configurations:**

**solenoidal magnetic field**

**dipole field**





**cylindrical symmetry**

**deflection in** *<sup>x</sup>***-** *<sup>y</sup>* **(** ρ **-** φ **) plane**

**tracking detectors arranged in cylindrical shells**

**measurement of curved trajectories in** ρ **-** φ **planes at fixed** ρ

#### **Dipole field**



**rectangular symmetry**

**deflection in** *y* **-** *<sup>z</sup>* **plane**

**tracking detectors arranged in parallel planes**

**measurement of curved trajectories**  in  $y$  -  $z$  planes at fixed  $z$ 

## **Tracking Systems: ATLAS**



## **Tracking Systems: CMS**



## **Tracking Systems: ATLAS & CMS**



#### **Momentum Measurement**



#### **orders of magnitude**

$$
P_{\perp} = 1 \, GeV
$$
  $B = 2 \, T$   $R = 1.67 \, m$   
 $P_{\perp} = 10 \, GeV$   $B = 2 \, T$   $R = 16.7 \, m$ 

**the sagitta** *<sup>s</sup>*



**assume a track length of 1** *<sup>m</sup>*

$$
P_{\perp} = 1 \text{GeV} \quad s = 7.4 \text{ cm}
$$

$$
P_{\perp} = 10 \text{GeV} \quad s = 0.74 \text{ cm}
$$

#### **Momentum Measurement**

**Once we have measured the transverse momentum and the dip angle the total momentum is**

$$
P = \frac{P_{\perp}}{\cos \lambda} = \frac{0.3BR}{\cos \lambda}
$$

**the error on the momentum is easely calculated**

$$
\frac{\partial P}{\partial R} = \frac{P_{\perp}}{R}
$$

$$
\frac{\partial P}{\partial \lambda} = -P_{\perp} \tan \lambda
$$

$$
\left(\frac{\Delta P}{P}\right)^2 = \left(\frac{\Delta R}{R}\right)^2 + (\tan \lambda \Delta \lambda)^2
$$

**We need to study**

**the error on the radius measured in the bending plane** ρ **-** φ

**the error on the dip angle in the** ρ **-** *<sup>z</sup>* **plane**

**We need to study also**

**contrubution of multiple scattering to momentum resolution**

#### **Comment:**

**in an hadronic collider the main emphasis is on transverse momentum**

**elementary processes among partons that are not at rest in the laboratory frame**

**use of momentum conservation only in the transverse plane**

## **The Helix Equation**

**The helix is described in parametric form**

$$
x(s) = x_o + R \left[ \cos \left( \Phi_o + \frac{h s \cos \lambda}{R} \right) - \cos \Phi_o \right]
$$

$$
y(s) = y_o + R \left[ \sin \left( \Phi_o + \frac{h s \cos \lambda}{R} \right) - \sin \Phi_o \right]
$$
  

$$
z(s) = z_o + s \sin \lambda
$$

λ **is the dip angle**  $h = +1$  is the sense of rotation on the helix **The projection on th** *<sup>x</sup>***-***<sup>y</sup>* **plane is a circle**

$$
(x - x_o + R\cos\Phi_o)^2 + (y - y_o + R\sin\Phi_o)^2 = R^2
$$

 $x_o$  and  $y_o$  the coordinates at  $s=0$ *Φ***o is also related to the slope of the tangent to the circle at**  $s = 0$ 



## **The Helix Equation**



$$
y(z) \approx y_o + \frac{1}{\tan \lambda} (z - z_o)
$$
  $y(z) = y_o + \text{ctan} \lambda (z - z_o)$  **straight line**

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 $\left( \, x_2^{}, y_2^{}, z_2^{}\, \right)$ 

 $(x_1, y_1, z_1)$ 

# **The Helix Equation**



## **Straight Line Fit**

**This is a well known problem a reference frame**  $\mathsf{N}{\texttt{+1}}$  measuring detetectors at  $z_0, \ldots, z_n, \ldots, z_N$ **a particle crossing the detectors**  $\mathsf{N}{\texttt{+1}}$  coordinate measurements  $\emph{y}_0,...,\emph{y}_n,...,\emph{y}_N$ **each measurement affected by uncorrelated**  $\mathsf{errors}\; \sigma_0, \! \dots, \sigma_n, \: ... , \! \sigma_N$ *a*

Find the best line  $y = a + b$  *z* that fit the track

**The solution is found by minimizing the** <sup>χ</sup>**<sup>2</sup>**

$$
a = (S_y S_{zz} - S_z S_{zy})/D
$$

$$
b = (S_1 S_{zy} - S_z S_y)/D
$$

**the covariance matrix (at**  $z = 0$ ) is

$$
\begin{pmatrix} \sigma_a^2 & c_{ab} \\ c_{ab} & \sigma_b^2 \end{pmatrix} = \frac{1}{D} \begin{pmatrix} S_{zz} & -S_z \\ -S_z & S_1 \end{pmatrix}
$$

depends only on 
$$
\sigma
$$
,  $z_n$  and  $N$ 



$$
\chi^{2} = \sum_{n=0}^{N} \frac{(y_{n} - a - bz_{n})^{2}}{\sigma_{n}^{2}}
$$

$$
S_1 = \sum_{n=0}^{N} \frac{1}{\sigma_n^2}
$$
  
\n
$$
S_y = \sum_{n=0}^{N} \frac{y_n}{\sigma_n^2}
$$
  
\n
$$
S_{zz} = \sum_{n=0}^{N} \frac{z_n}{\sigma_n^2}
$$
  
\n
$$
S_{yz} = \sum_{n=0}^{N} \frac{y_n z_n}{\sigma_n^2}
$$
  
\n
$$
D = S_1 S_{zz} - S_z S_z
$$

## **Straight Line Fit: Matrix Formalism**

**It is useful to restate the problem using a matrix formalism [4:Avery 1991]**

**This is useful because:**

**it is more compact**

**it is easely extensible to other linear problems**

**it is more useful to formulate an iterative procedure**

**With the same assumption as before the linear model is given by**  $f = Ap$ 

$$
\mathbf{f} = \begin{pmatrix} f_0 \\ \dots \\ f_N \end{pmatrix} = \begin{pmatrix} a + bz_0 \\ \dots \\ a + bz_N \end{pmatrix} = \begin{pmatrix} 1 & z_0 \\ 1 & \dots \\ 1 & z_N \end{pmatrix} \begin{pmatrix} a \\ b \end{pmatrix} = \mathbf{A}\mathbf{p}
$$

$$
\mathbf{Y} = \begin{pmatrix} y_0 \\ y_0 \\ \dots \\ y_N \end{pmatrix} \quad (\mathbf{V})_{ij} = \left\langle (y_i - \left\langle y_i \right\rangle)(y_j - \left\langle y_j \right\rangle) \right\rangle
$$

$$
(\mathbf{V})_{ij} = \sigma_i^2 \delta_{ij} \quad \boxed{\text{if uncorrelated}}
$$

**The**  <sup>χ</sup>**<sup>2</sup> can be written as**

$$
\chi^2 = (\mathbf{Y} - \mathbf{A}\mathbf{p})^T \mathbf{W} (\mathbf{Y} - \mathbf{A}\mathbf{p}) \qquad \mathbf{W} = \mathbf{V}^{-1}
$$

**The minimum**  <sup>χ</sup>**<sup>2</sup> is obtained by**

$$
\boxed{\tilde{\mathbf{p}} = \left(\mathbf{A}^T \mathbf{W} \mathbf{A}\right)^{-1} \mathbf{A}^T \mathbf{W} \mathbf{Y}}
$$

**The covariance matrix of the parameters is obtained from the measurements covariance matrix** *V*

$$
\boxed{\mathbf{V}_{\mathbf{P}}=\left(\mathbf{A}^{T}\mathbf{V}^{-1}\mathbf{A}\right)^{-1}}
$$

**please notice (** *N***+1 measurements,**  *M* **parameters )**

 $\textsf{dimensions A} \quad = (N{+}1) \times M$  $\textsf{dimensions V} \quad = (N{+}1) \times (N{+}1)$  $\boldsymbol{A}^{\text{T}}\boldsymbol{\mathrm{W}}\boldsymbol{\mathrm{A}} = M \times M$  $\textsf{dimensions} \ \ \mathrm{A}^{\text{T}}\textbf{W} \quad = M \times (N{+}1)$  $\textbf{d}$ **imensions**  $\textbf{V}_{\text{p}}$   $\textbf{v} = M$ ×*M*

## **Straight Line Fit**



**The** *S* **are easily computed in finite form**

$$
S_1 = \frac{N+1}{\sigma^2} \qquad S_z = (N+1)\frac{z_c}{\sigma^2}
$$

$$
S_{zz} = \frac{N+1}{\sigma^2} \left[ \frac{(N+2) L^2}{N} + z_c^2 \right]
$$

$$
D = \frac{L^2}{12\sigma^4} \frac{(N+1)^2 (N+2)}{N}
$$

**The errors on the intercept and the slope are**

$$
\sigma_a^2 = \left[1+12\frac{N}{N+2}\frac{z_c^2}{L^2}\right]\frac{\sigma^2}{N+1}
$$

$$
\sigma_b^2 = \frac{\sigma^2}{(N+1)L^2} \frac{12N}{(N+2)}
$$

#### **important features:**

**both errors are linearly dependent on the measurement error** <sup>σ</sup>

 $\mathbf{b}$ oth errors decrease as  $1/\sqrt{N}+1$ 

**the error on the slope decrease as of the lever arm** *L*

**the error on the intercept increases if** *zc***increase**

 $S$  and errors: all computed at  $z=0$ 

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#### **Errors At The Center Of The Track**





#### **It is easely seen that for uniform spacing and equal errors**

$$
S_1 = \frac{N+1}{\sigma^2} \underbrace{\left(S_z = 0\right)}_{D} S_{zz} = \frac{N+1}{\sigma^2} \left[ \frac{(N+2) L^2}{N} \right]
$$

$$
D = \frac{L^2}{12\sigma^4} \frac{(N+1)^2 (N+2)}{N}
$$

*S***1 and** *D* **do not change**  $S_z$  and  $S_{zz}$  change

**The errors are now**



**The intercept is different from the previous case (origin at**  $z = 0$ )

**Obviously, taking properly into account error propagation ve get the same result for the impact parameter** *ip*

$$
ip = f(-z_c) = a - bz_c
$$

$$
\sigma_{ip}^2 = \sigma_a^2 + z_c^2 \sigma_b^2
$$
 
$$
\begin{array}{|l|}\n\hline\n\sigma_a \text{ and } \sigma_b \text{ uncorrela-} \\
\hline\n\text{ted if origin at } z_c\n\end{array}
$$

$$
\sigma_{ip}^2 = \frac{\sigma^2}{N+1} + \frac{\sigma^2}{N+1} \frac{12N}{N+2} \frac{z_c^2}{L^2}
$$

### **Vertex Detectors**

**The previous result shows clearly the need for vertex detectors to achieve a precise measurements of the impact parameter**



**The "amplitude" of the error is determined by the error on the slope** <sup>σ</sup>**/***<sup>L</sup>* **by the distance of the point to which**   $\bm{w}$ e extrapolate  $\; z_c/L$ **by the size of the measurement error**



**We should have**

**small measurement errors** <sup>σ</sup> **large lever arm** *<sup>L</sup>*

**place first plane as near as possible**  to the production point: small  $z_c$ 

**Increasing the number of points also**  improves but only as  $\sqrt{N}+1$ 

**The technology used is silicon detectors with resolution of the order of** <sup>σ</sup> **~ 10** <sup>µ</sup>*<sup>m</sup>*

**expensive small** *N***small** *L*

### **Vertex Detectors**

**Summarizing:the error on the impact parameter is**

$$
\sigma_{ip}\,=\,Z\,(\,r\,,N\,)\frac{\sigma}{\sqrt{N+1}}
$$

**for the ATLAS pixel detector**

$$
N{+}1=3,\,\sigma=10\,\,\mu m
$$

$$
z_0 = 4.1 \, \, cm, \, z_2 = 13.5 \, \, cm
$$

$$
L=9.4,\,z_c{=}6.8,\,r=0.72
$$

$$
\sigma_{ip}=12\,\,\mu m
$$



$$
Z\left(r,N\right)=\sqrt{1+12\frac{N}{N+2}r^{2}}\left\vert
$$



### **Vertex Detector + Central Detector**

#### **We have seen that the error on the impact parameter is**

 $\sigma_{ip}^2\,=\sigma_a^2\,+\,z_c^2\!\!\left[\!\sigma_b^2\right]$ 



**The first term:**

```
depend only on the precision of the 
vertex detector
```

```
it is equivalent to a very precise
measurement (σa ~ 5 µm) very near
to the primary vertex (z_c)
```
**The second term depends on the error on the slope and is limited by the small lever arm** *L* **typical of vertex detectors (~ 10** *cm***)**

**It is usually very expensive to increase this lever arm**

**A solution is a bigger detector (Central Detector) less precise (usually less expensive) but with a much bigger lever arm** *L*

> **The error on the slope then become smaller**

**The error on the extrapolation become smaller**

**This is the arrangement usually adopted by experiments who want to measure the impact parameter**



#### **Momentum Measurement: Sagitta**

**To introduce the problem of momentum measurement let's go back to the sagitta**

**a particle moving in a plane perpendicular to a uniform magnetic field** *<sup>B</sup>*

$$
R = \frac{p}{0.3B} \qquad \frac{\delta p}{p} = \frac{\delta R}{R}
$$

the trajectory of the particle is an arc of **of length** *<sup>L</sup>*



**assume we have 3 measurements:**  $y_1$ ,  $y_2$ ,  $y_3$ 

$$
s = y_3 - \frac{y_1 + y_2}{2} \quad \delta s = \sqrt{\frac{3}{2}} \delta y \sim \delta y
$$

**the error on the radius is related to the sagitta error by**

$$
|\delta s| = \frac{L^2}{8R} \frac{\delta R}{R} \sim \delta y \qquad \frac{L^2}{8R} \frac{\delta p}{p} = \delta y
$$

$$
\frac{\delta p}{p} = \frac{8R}{L^2} \delta y \qquad \frac{\delta p}{p} = \frac{8p}{0.3BL^2} \delta y
$$

$$
\frac{\delta p}{p^2} = \frac{8\delta y}{0.3BL^2}
$$

#### **important features**

**the percentage error on the momentum is proportional to the momentum itself**

**the error on the momentum is inversely proportional to** *<sup>B</sup>*

**the error on the momentum is inverse**ly proportional to  $1/L^2$ 

**the error on the momentum is proportional to coordinate measurement error**

# **Tracking In Magnetic Field**

**The previous example showed the basic features of momentum measurement**

**Let's now turn to a more complete treatement of the measurement of the charged particle trajectory**

**We have already seen that for an homogeneus magnetic field the trajectory projected on a plane perpendicular to the magnetic field is a circle**

$$
(y - y_o)^2 + (x - x_o)^2 = R^2
$$



**for not too low momenta we can use a linear approximation**

$$
y = y_o + \sqrt{R^2 - (x - x_o)^2}
$$
  
\n
$$
y \approx y_o + R \left( 1 - \frac{(x - x_o)^2}{2R^2} \right)
$$
  
\n
$$
y = \left( y_o + R - \frac{x_o}{2R^2} \right) + \frac{x_o}{R} x - \left( \frac{1}{2R} \right) x^2
$$

**we are led to the parabolic approximation of the trajectory**

$$
y = a + bx + cx^2
$$

**let's stress that as far as the track parameters is concerned the dependence is linear**

**The parameters** *a,b,c* **are**

**intercept at the origin slope at the origin radius of curvature (momentum)**

### **Quadratic Fit**





**However we can use the matrix formalism developed for the straight line:**

$$
\mathbf{Y} = \begin{pmatrix} y_o \\ \dots \\ y_N \end{pmatrix} \quad \mathbf{p} = \begin{pmatrix} a \\ b \\ c \end{pmatrix} \qquad \mathbf{A} = \begin{pmatrix} 1 & x_0 & x_0^2 \\ \dots & \dots & \dots \\ 1 & x_N & x_N^2 \end{pmatrix} \quad \mathbf{W} = \begin{pmatrix} \frac{1}{\sigma_0^2} & 0 & 0 \\ 0 & \dots & \dots & 0 \\ 0 & 0 & \frac{1}{\sigma_N^2} \end{pmatrix}
$$

**let's recall the solution**

$$
\tilde{\mathbf{p}} = (\mathbf{A}^T \mathbf{W} \mathbf{A})^{-1} \mathbf{A}^T \mathbf{W} \mathbf{Y}
$$

$$
(\mathbf{A}^T \mathbf{W} \mathbf{A})^{-1} = \begin{pmatrix} F_0 & F_1 & F_2 \\ F_1 & F_2 & F_3 \\ F_2 & F_3 & F_4 \end{pmatrix}^{-1} F_k = \sum_{n=0}^N \frac{x_n^k}{\sigma_n^2}
$$

$$
\mathbf{A}^T \mathbf{W} \mathbf{Y} = \begin{pmatrix} M_0 \\ M_1 \\ M_2 \end{pmatrix} \qquad M_k = \sum_{n=0}^N \frac{y_n x_n^k}{\sigma_n^2}
$$

**The detectors are placed at positions**  $x_0, \dots, x_n, \dots, x_N$ **A track crossing the detectors** gives the measurements  $y_0$ , …,  $y_n$ , …,  $y_N$ **Each measurement has an error** σ<sub>n</sub> **Using the parabola approximation, the track parameters are found by minimizing the** χ**<sup>2</sup>**

$$
\chi^{2} = \sum_{n=0}^{N} \frac{(y_{n} - a - bx_{n} - cx_{n}^{2})^{2}}{\sigma_{n}^{2}}
$$

#### **Quadratic Fit**

**The result is [4: Avery 1991, Blum-Rolandi 1993 p.204, Gluckstern 63]**

$$
a = \frac{\sum y_n G_n}{\sum G_n} \quad b = \frac{\sum y_n G_n}{\sum x_n G_n} \quad c = \frac{\sum y_n G_n}{\sum x_n^2 G_n}
$$
  

$$
G_n = F^{11} - x_n F^{21} + x_n^2 F^{31}
$$
  

$$
P_n = -F^{12} + x_n F^{22} - x_n^2 F^{32}
$$
  

$$
Q_n = F^{13} - x_n F^{23} + x_n^2 F^{33}
$$

**The quantities** *Fij* **are the determinants of the 2x2 matrices obtained from the 3x3 matrix** *<sup>F</sup>* **by removing row** *<sup>i</sup>***, column** *j*

**The covariance matrix**

$$
\mathbf{V}_{\mathbf{p}} = (\mathbf{A}^{T} \mathbf{W} \mathbf{A})^{-1} = \begin{bmatrix} F_{0} & F_{1} & F_{2} \\ F_{1} & F_{2} & F_{3} \\ F_{2} & F_{3} & F_{4} \end{bmatrix}^{-1}
$$

**The result can be found in [Blum-Rolandi, p. 206]**

**To get some idea of the covariance matrix let's first compute it by setting the origin at the center of the track**

$$
x_c = \sum_{n=0}^{N} \frac{x_n}{N+1}
$$

**with this choice one can "easely" find**

$$
F_1 = F_3 = 0
$$
  
\n
$$
F_0 = \frac{N+1}{\sigma^2}
$$
  
\n
$$
F_2 = \frac{L^2}{\sigma^2} \frac{(N+1)(N+2)}{12N}
$$
  
\n
$$
F_4 = \frac{L^4}{\sigma^2} \frac{(N+1)(N+2)(3N^2+6N-4)}{240N^3}
$$
  
\n
$$
S = F_0F_4 - F_2^2 = \frac{L^4}{\sigma^4} \frac{(N-1)(N+1)^2(N+2)(N+3)}{180N^3}
$$

**The covariance matrix is** 

$$
\mathbf{V}_{\mathbf{p}} = \frac{1}{F_0 F_4 - F_2 F_2} \begin{bmatrix} F_4 & 0 & -F_2 \ 0 & \frac{F_0 F_4 - F_2 F_2}{F_2} & 0 \ -F_2 & 0 & F_0 \end{bmatrix}
$$

**we are mostly interested on the error on the curvature**

$$
\sigma_c^2 = \frac{F_0}{F_0 F_4 - F_2 F_2} = \frac{\sigma^2}{L^4} C_N
$$

$$
C_N = \frac{180N^3}{(N-1)(N+1)(N+2)(N+3)}
$$

**it can be shown that the error on the curvature do not depend on the position of the origin along the track**

**Let's recall from the discussion on the sagitta**

$$
R = \frac{p}{0.3B} \qquad \frac{\delta p}{p} = \frac{\delta R}{R}
$$

**also recall that**

*c*

$$
c = \frac{1}{2R} \qquad \sigma_c = \frac{1}{2R^2} \delta R
$$

**and finally the momentum error**

$$
\boxed{\frac{\delta p}{p^2} = \frac{\sigma}{0.3 BL^2} \sqrt{4 C_N}}
$$

**the formula shows the same basic features we noticed in the sagitta discussion**

**we have also found the dependence on the number of measurements (weak)**

**We stress again that a good momentum resolution call for a long track**



**any trick that can extend the track length can produce significant improvements on the momentum resolution**

**the use of the vertex can also improve momentum resolution:**

**the common vertex from which all the tracks originate can be fitted the point found can be added to every track to extend the track length at**   $R_{min} \rightarrow 0$ 

**the position of the beam spot can also be used as constraint**

**Extending** *Rmax* **can be very expensive**







#### **Slope And Intercept Resolution**

**For completeness we give also the errors on the slope and intercept**

**The error on the slope is given by**

$$
\sigma_b^2 = \frac{1}{F_2} = B_N \frac{\sigma^2}{L^2}
$$

$$
B_N = \frac{12N}{(N+1)(N+2)}
$$

**We find the same qualitative behaviour we had for the straight line fit**

**The error on the intercept is**

$$
\sigma_a^2 = \frac{F_4}{F_0 F_4 - F_2 F_2} = A_N \sigma^2
$$

$$
A_N = \frac{3(3N^2 + 6N - 4)}{4(N-1)(N+1)(N+3)}
$$

**The only off diagonal element of the covariance matrix different from 0 is between intercept and curvature and we have**

$$
\sigma_{ac} = -\frac{F_2}{F_0 F_4 - F_2 F_2} = -D_N \frac{\sigma^2}{L^2}
$$

$$
D_N = -\frac{15N^2}{(N-1)(N+1)(N+3)}
$$

## **Extrapolation To Vertex**

**We want now compute the extrapolation to vertex and compare the behaviour of the results of the fit:**

**inside magnetic field**

**no magnetic field**

**having measured the parameters** *a,b,c* **at the center of the track, the intercept is**

 $y_{ip} = a + bx_v + cx_v^2$ 

**Propagation of the errors gives**

$$
\sigma_{ip}^2 = \sigma_a^2 + x_v^2 \sigma_b^2 + x_v^4 \sigma_c^2 + 2x_v^2 \sigma_{ac}
$$

**The calculation gives [Blum-Rolandi 1993]**

$$
\sigma_{ip} = \frac{\sigma}{\sqrt{N+1}} B_{aa}(r, N)
$$

where  $B_{aa}(r,N)$  is analogous to  $Z(r,N)$ **defined for the straight line fit (see next slide for a table of values)**



**let's compare the error assuming the geometry of the ATLAS pixel detector:**

 $R_{min} = 4.7,\, R_{max} = 13.5,\, N{+}1 = 3$ 

we have  $r = 1$  and from the 2 tables we get

$$
B_{aa}(1,2)\,=\,7.63\\Z(1,2)\,=\,2.65
$$

**We see that the error is degraded by a factor ~ 2.9**

**The reason is that the error on momentum cause an additional contribution to the error in the extrapolation**

**a central tracking detector is needed**

$$
\sigma_{ip} = \frac{\sigma}{\sqrt{N+1}} B_{aa}(r, N)
$$

#### $B_{aa}$  (  $r, N$  )





### **Parameters Propagation**

**We have seen that changing the origin of the reference frame**

> **the track parameters change the covariance matrix changes**

**It is often useful to propagate the parameters describing the track from one "origin" (point 0) to "another" (point 1 )**

**For linear models this is very easely expressed in matrix form**

$$
\mathbf{p}_{i} = \mathbf{f}_{i}(\mathbf{p}_{k}) = \mathbf{D}_{i}\mathbf{p}_{k} \qquad \mathbf{D}_{i} = \frac{\partial \mathbf{f}_{i}}{\partial \mathbf{p}_{i}}
$$

 $\mathbf{v}_k$  or  $\mathbf{v}_k$  better understand the above formulas **let's apply them to the straight line and to the parabola**





 $0\quad 0\quad 1$ 

**Using the matrix**  *D* **we can also propagate the covariance matrix of the parameters**

$$
\mathbf{V}_{1}=\left(\mathbf{D}^{\mathrm{T}}\mathbf{V}_{0}^{-1}\mathbf{D}\right)^{-1}
$$

**Particles moving through the detector material suffer innumerable EM collisions which alter the trajectory in a random fashion (stochastic process)**



#### **Few examples:**



**consider a 10** *GeV* **pion**



**The effect goes as 1/***p***: for a pion of 1** *GeV* **the effect is <sup>10</sup> times larger**

**The lateral displacement is proportional to the thickness of the detector: usually can be neglected for thin detectors**

**In what follow we will consider only thin detectors**

**For thick detectors ( for example large volume gas detectors) see [Gluckstern 63 Blum-Rolandi 93, Block et al. 90]**

**The scattering angle has a distribution that is almost gaussian**



**At large angles deviations from gaussian distributions appear that manifest as a long tail going as**  $\sin^{-4}\theta/2$ 

**In thick detectors the distribution of the lateral displacement should also be considered**

**The joint distribution of the scattering angle and the lateral displacement is**

$$
\boxed{P\left(\varepsilon_p,\theta_p\,\right)=\frac{\sqrt{3}}{\pi\left<\theta_p^2\,\right>X^2}\exp\Biggl[-\frac{2}{\left<\theta_p^2\right>}\Biggl(\theta_p^2-\frac{3\varepsilon_p\theta_p}{X}+\frac{3\varepsilon_p^2}{X^2}\Biggr)\Biggr]}
$$

**Multiple scattering is a cumulative effect and introduces correlation among the coordinate measurements**

**The treatment of multiple scattering is different for:**

**discrete detectors**

**continous detectors**

**Here we consider only the simplest case of discrete and thin detectors**

**For continous detectors see for example [5: Avery 1991]**

**Let's consider 3 thin detectors**



**A track cross the 3 planes at positions**  $\tilde{y}_i$   $\tilde{y}_j$   $\tilde{y}_k$ 

**The 3 coordinate have measurement errors** <sup>σ</sup>*i***,** σ*j***,** σ*<sup>k</sup>* **due to the detector resolution**

**They also have mean value**

$$
\big<\, \tilde y_i\, \big> = \, \overline{\tilde y}_i \quad \big<\, \tilde y_j\, \big> = \, \overline{\tilde y}_j \quad \big<\, \tilde y_k\, \big> = \, \overline{\tilde y}_k
$$

on plane  $\boldsymbol{i}$   $\ \ y_{_{\boldsymbol{i}}} = \tilde{y}_{_{\boldsymbol{i}}}$ 

**Because of multiple scattering on plane** *<sup>i</sup>* **the actual trajectory cross plane** *j* **at**

$$
y_j = \tilde{y}_j + (z_j - z_i) \delta \theta_i
$$

**Because of multiple scattering on planes**  *i,j* **the actual trajectory cross plane** *<sup>k</sup>***at**

$$
y_k\,=\,\tilde{y}_k\,+\big(\,z_k\,-\,z_i\,\big)\delta\theta_i\,+\big(\,z_k\,-\,z_j\,\big)\delta\theta_j
$$

**Since** $\delta\theta$   $\rangle = 0$ 

$$
\overline{y}_i = \overline{\tilde{y}}_i \qquad \overline{y}_j = \overline{\tilde{y}}_j \qquad \overline{y}_k = \overline{\tilde{y}}_k
$$

**we can now compute the covariance matrix of the coordinate measurements including multiple scattering**

$$
V_{nm} = \langle (y_m - \overline{y}_m)(y_n - \overline{y}_n) \rangle
$$

**First the diagonal elements**

$$
V_{ii} = \left\langle \left(y_i - \overline{y}_i\right)^2 \right\rangle = \left\langle \left(y_i - \overline{\tilde{y}}_i\right)^2 \right\rangle
$$

$$
\frac{V_{ii} = \sigma_i^2}{V_{jj}} = \left\langle \left(y_j - \overline{y}_j\right)^2 \right\rangle = \left\langle \left(y_j - \overline{\tilde{y}}_j + \left(z_j - z_i\right)\delta\theta_i\right)^2 \right\rangle
$$
  
\n
$$
= \left\langle \left(y_j - \overline{\tilde{y}}_j\right)^2 \right\rangle + \left(z_j - z_i\right)^2 \left\langle \delta\theta_i^2 \right\rangle + 2\left(z_j - z_i\right) \left\langle \delta\theta_i\right\rangle
$$
  
\n
$$
V_{jj} = \sigma_j^2 + \left(z_j - z_i\right)^2 \left\langle \delta\theta_i^2 \right\rangle
$$

~ *iy*

 $\boldsymbol{y}_{i}$ 

~  $\boldsymbol{y}_j$ 

 $y_i$ 

*i* **δθ**

**it easy to verify that**

$$
\boxed{V_{kk}\,=\,\sigma_k^2+\left(\,z^{\phantom{k}}_k\,-\,z^{\phantom{k}}_i\,\right)^2\left<\,\delta\theta_i^2\,\right>+\left(\,z^{\phantom{k}}_k\,-\,z^{\phantom{k}}_j\,\right)^2\left<\,\delta\theta_j^2\,\right>}
$$

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~  $\bm{y}_{\bm{k}}$ 

 $y_{k}$ 

*<sup>j</sup>* **δθ**

$$
\boxed{V_{nm} = \langle (y_m - \overline{y}_m)(y_n - \overline{y}_n) \rangle}
$$
\n
$$
V_{ij} = \langle (y_i - \overline{y}_i)(y_j - \overline{y}_j) \rangle = \langle (y_i - \overline{\hat{y}}_i)(y_j - \overline{\hat{y}}_j + (z_j - z_i)\delta\theta_i) \rangle
$$
\n
$$
V_{ik} = \langle (y_i - \overline{y}_i)(y_k - \overline{y}_k) \rangle
$$
\n
$$
= \langle (y_i - \overline{\hat{y}}_i)(y_k - \overline{\hat{y}}_k + (z_k - z_i)\delta\theta_i + (z_k - z_j)\delta\theta_j) \rangle
$$
\n
$$
V_{jk} = \langle (y_j - \overline{y}_j)(y_k - \overline{y}_k) \rangle
$$
\n
$$
= \langle (y_j - \overline{y}_j)(y_k - \overline{y}_k) \rangle
$$
\n
$$
= \langle (y_j - \overline{y}_j)(z_k - \overline{y}_k) \rangle
$$
\n
$$
= \langle (y_j - \overline{y}_j + (z_j - z_i)\delta\theta_i)(y_k - \overline{y}_k + (z_k - z_i)\delta\theta_i + (z_k - z_j)\delta\theta_j) \rangle
$$
\n
$$
= \langle (z_j - z_i)\delta\theta_i(z_k - z_i)\delta\theta_i \rangle
$$
\n
$$
\boxed{V_{jk} = (z_j - z_i)(z_k - z_i)\delta\theta_i}
$$

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~  $y_{k}$ 

#### **Summarizing, the covariance matrix is**

$$
V = \begin{pmatrix} \sigma_i^2 & 0 & 0 \\ 0 & \sigma_j^2 & 0 \\ 0 & 0 & \sigma_k^2 \end{pmatrix} + \begin{pmatrix} 0 & 0 & 0 \\ 0 & \left(z_j - z_i\right)^2 \delta \theta_i^2 & \left(z_k - z_i\right) \left(z_j - z_i\right) \delta \theta_i^2 \\ 0 & \left(\overline{z_k} - \overline{z_i}\right) \left(\overline{z_j} - \overline{z_i}\right) \delta \theta_i^2 & \left(z_k - z_i\right)^2 \delta \theta_i^2 + \left(z_j - z_i\right)^2 \delta \theta_j^2 \end{pmatrix}
$$

#### **The second matrix has**

**diagonal elements due to any previous material affecting the trajectory impact point at the given plane**

**off diagonal elements: only presents if a previous material layer affects at the same time the trajectory impact points for the 2 planes the same scattering at plane** *<sup>i</sup>* affects the trajectory at plane  $\hat{J}$  and plane  $\hat{k}$ ~ *i y* ~  $\boldsymbol{y}_j$  $\tilde{\phantom{a}}$ *k y*  $\boldsymbol{y}_i$  $y_{i}$  $y_{k}$ *i* **δθ** *<sup>j</sup>* **δθ**

 $z_i$ 

 $z_j$  *z j z k* 

# **Track Fit With Multiple Scattering**

**The methods developed to fit a track to the measured points can be used to perform a fit taking into account M.S.**

**the covariance matrix is computed**

**the same fit procedure is applied**

**Let's now try to understand qualitatively the effect of multiple scattering on the determination of tracks parameters:**

> **the size of the effect goes as 1/***<sup>p</sup>* **then the effect is important for low momentum track**

**Assume we are dominated by multiple scattering**

**the momentum resolution is given by**

$$
\left|\frac{\delta p}{p^2} = \frac{\sigma}{0.3 B L^2} \sqrt{4 A_N}\right|
$$

**the coordinate error due to M.S. is** 



**we have then**



**We conclude:**

**for low momentum the percentage momentum resolution reach a almost constant value (still dependent on** β**)**

> $\frac{\delta p}{\delta}$   $\rightarrow$  constant *p*

**The momentum resolution only improves as 1/***<sup>L</sup>*

**The additional factor 1/***<sup>N</sup>* **can help but in this case uniform spacing is essential** 

#### **Momentum Resolution with M.S.**



## **Track Fit With Multiple Scattering**

**Same kind of considerations for the error on the slope and on the intercept**

**the multiple scattering error is**

$$
\sigma \sim \frac{L}{N} \delta \theta = \frac{L}{N} \frac{0.0136}{p\beta} \sqrt{\frac{X}{X_o}}
$$

**the error on the slope is** 

$$
\sigma_b = \sqrt{B_N} \frac{\sigma}{L}
$$

$$
\sigma_b = \sqrt{B_N} \frac{L}{LN} \frac{0.0136}{p\beta} \frac{X}{X_o}
$$

$$
\sigma_b\,=\,\frac{\sqrt{B_N}}{N}\frac{0.0136}{p\beta}\sqrt{\frac{X}{X_o}}
$$

**we cannot improve anymore the error on the slope (direction) by increasing the lever arm**

> **the limit is set by the multiple scattering angle itself**

**As far as the impact parameter resolution**

$$
\sigma_{ip} = \frac{\sigma}{\sqrt{N+1}} B_{aa}(r, N)
$$

$$
\sigma_{ip}^{} = \frac{B_{aa}^{} \left(r, N\right)}{\sqrt{N+1}} \frac{L}{N} \frac{0.0136}{p\beta} \sqrt{\frac{X}{X_o}}
$$

**large lever arm degrade the impact parameter resolution**

> **for a given error on the slope set by the multiple scattering angle the error on the extrapolation goes as the lever arm**

**Unfortunately both ATLAS and CMS have a lot of material**

**silicon detectors for high precision silicon for radiation hardness silicon for rate capabilities**

## **Material in ATLAS**



## **Tracker Resolutions With M.S.**

**We have seen that for low momentum track the momentum resolution and the impact parameter resolution are dominated by multiple scattering**

**the momentum resolution tend to**

$$
\frac{\delta p}{p^2} \to \frac{k_p}{p} \sqrt{\frac{X}{X_o}} \qquad \frac{\delta p}{p^2} \to \frac{K_p}{p \sqrt{\sin \theta}}
$$

**the impact parameter resolution tend to**

$$
\boxed{\sigma_{ip}^{}\ \to \frac{k_{ip}^{}}{p}\sqrt{\frac{X}{X_o} \qquad \sigma_{ip}^{}\ \to \frac{K_{ip}^{}}{p\sqrt{\sin\theta}}}
$$

**The amount of material actually traversed by the particles depend on the polar angle**



**Since the multiple scattering error and the measurement error are independent to total error is sum in quadrature of the 2 term**

**For the ATLAS detector montecarlo studies have shown that the resolutions can be parametrised as**

$$
\sigma_{ip} = 11 \oplus \frac{73}{p_{\perp} \sqrt{\sin \theta}} \qquad [\mu m]
$$

$$
\sigma_{ip} \rightarrow \frac{k_{ip}}{p} \sqrt{\frac{X}{X_o}} \qquad \sigma_{ip} \rightarrow \frac{K_{ip}}{p \sqrt{\sin \theta}} \qquad \qquad \boxed{\frac{\delta p_\perp}{p^2_\perp}} = 0.00036 \oplus \frac{0.013}{p_\perp \sqrt{\sin \theta}} \qquad \left[ GeV^{-1} \right]
$$



### **Sign Of The Charge**

**The sign of the charge is defined by the sign of 1/***<sup>R</sup>*



**This measurement becomes more and more difficult as the momentum increases**

**Let's find up to which momentum the ATLAS tracker will be able to measure the sign of a charged particle**

**We recall taht the error on the radius as determined from the parabola fit is**

$$
\sigma_c^2 = \frac{\sigma^2}{L^4} C_N
$$

**We remember that in our exemple we had**

$$
C_N = 12, L = 75 \; cm, s = 20 \; \mu m
$$

**if we require a 3** <sup>σ</sup> **identification**

$$
\frac{1}{R} > 3\sigma_{\frac{1}{R}} = 6\sigma_c = \frac{3\sigma_y}{L^2} \sqrt{4C_N}
$$

$$
\frac{1}{0.3BR} > \frac{3\sigma_y}{0.3BL^2} \sqrt{4C_N}
$$

$$
\boxed{p < \frac{0.3 BL^2}{3 \sqrt{4 C_N} \sigma_y}}
$$

#### **inserting numerical values we find**

 $p < 800 \ GeV$ 

#### **Systematic Effects**

**Recall the formulas we found for the parabola fit**

$$
a = \frac{\sum y_n G_n}{\sum G_n} \quad b = \frac{\sum y_n G_n}{\sum x_n G_n} \quad c = \frac{\sum y_n G_n}{\sum x_n^2 G_n}
$$

**Using those formulas it is easy to evaluate systematic effects on the track parameters due to systematic errors on the position measurements**

#### **Examples:**

**displacement of vertex detector with respect to the central detector**



**Inserting, for example, in the formula for the curvature** 3

$$
c = \frac{\sum y_n G_n}{\sum x_n^2 G_n} \underbrace{\left(\sum_{n=0}^{\infty} G_n\right)}_{\sum x_n^2 G_n} \equiv c_{true} + \delta c
$$

**a more sofistcated effect could be the rotation of the vertex detector**



$$
y_0 \rightarrow y_0 + \delta_0 \quad y_1 \rightarrow y_1 + \delta_1 \quad y_2 \rightarrow y_2 + \delta_2
$$

$$
c = \frac{\sum y_n G_n}{\sum x_n^2 G_n} \left( \frac{\sum_{n=0}^{3} \delta_n G_n}{\sum x_n^2 G_n} \right) \equiv c_{true} + \delta c
$$

### **Systematic Effects: Misalignment**

**Let's assume that one measurement is systematically displaced: misalignment or distortion (systematic error)**



**Recall the formula for the radius from the parabola fit**

$$
\frac{1}{2R} = \frac{\sum y_n G_n}{\sum x_n^2 G_n}
$$

**introducing the coordinate with error**

$$
\frac{1}{2R} = \frac{\sum y_n G_n}{\sum x_n^2 G_n} + \frac{G_k}{\sum x_n^2 G_n} \delta
$$

$$
\frac{1}{2R} = \frac{1}{2R_{true}} + \frac{G_k}{\sum x_n^2 G_n} \delta \quad \boxed{\Delta \frac{1}{R} \sim 2 \frac{\delta}{L^2}}
$$

**the second term is the systematic effect on the radius due to the systematic error on the measurement** Since the coefficients  $\boldsymbol{G}_k$  are know the **effect can be precisely estimated Please notice**

> **the sign of the systematic error on**  1/ $R$  is fixed by the sign of  $\delta$

$$
Q = +1 \frac{1}{R} > 0 \qquad Q = -1 \frac{1}{R} < 0
$$



## **Systematic Effects: Misalignment**

**As an example consider a systematic effect as seen in the ALEPH TPC**

**The resolution was studied using muon pairs produced in** *e***+** *e***- annihilation at the**   $Z^0$  **peak** 

**The muon are produced back to back and have exactly half the c.m. energy each**

**The plot show the momentum reconstructed separately for positive and negative muons**

**As the plot clearly show the error is quite large**

To account for this error  $\delta \sim 1$   $mm$ !

**Magnetic field distortion**

**A correction procedure is the essential**

**The following plot shows the same distribution after proper magnetic distortion corrections are applied**



## **Problems With The Fit Procedure**

**We have learned how to use linear models to fit the projection of the charged particle track**

**The method could be extendend to non linear problems (inhomogeneous magnetic field) by linearization and iteration**

**The solution of the problem is given by**

$$
\tilde{\mathbf{p}} = \left(\mathbf{A}^T \mathbf{W} \mathbf{A}\right)^{-1} \mathbf{A}^T \mathbf{W} \mathbf{Y} \qquad \mathbf{W} = \mathbf{V}^{-1}
$$

**to solve the problem the matrix** *V* **has to be inverted**

```
easy if V diagonal ( time O(n) )
```
**We have seen that multiple scattering introduces correlation among measurements and makes** *V* **non diagonal**

```
For large detectors the dimension of V
can be prohibitively large (time O(n^3))
```
**The fit is normally used to rank track candidates during pattern recognition**

**The fit procedure gives the track parameters at a given surface or plane**



**Often prediction of the track crossing point at a different plane is needed**

**impact parameter**

**match with calorimeters**

**match with particle ID (RICH)**

**The fit procedure described is not optimal for this problem:**

> **multiple scattering makes prediction (extrapolation) non optimal**



**to start the Kalman Filter we need a seed the position on the next plane is predicted the measurement is considered prediction and measurement are merged (filtered) then new prediction … measurement … filtering … prediction … measurement …**

**filtering … prediction … measurement …**

**The filtered trajectory The smoothed trajectory**



**The filtering is nothing but a weighted average of the**

**new measurement** *yn*

the prediction 
$$
y_p
$$
  
\n
$$
y_f = \frac{\frac{1}{\sigma_p^2} y_p + \frac{1}{\sigma_n^2} y_n}{\frac{1}{\sigma_p^2} + \frac{1}{\sigma_n^2}}
$$
\n
$$
y_f = \frac{\sigma_n^2}{\sigma_p^2 + \sigma_n^2} y_p + \frac{\sigma_p^2}{\sigma_p^2 + \sigma_n^2} y_n
$$

**Clearly if the new measurement has a very large error**

 $\sigma_n \to \infty$  *y<sub>f</sub>*  $\to y_p$ 

**measurement ignored**

**If the prediction has a large error (for example large multiple scattering)**

 $\sigma_p \rightarrow \infty$  *y*<sub>f</sub>  $\rightarrow y_n$ 

**prediction ignored**

**The effect of multiple scattering, or any other stochastic effect, can be handled in the prediction**

**The advantages of this procedure are**

**is an iterative procedure**

**not necessary to invert large matrices**

**is a local procedure: at any step the estimate at the given plane is the best that make use of the prevoius measurements**

**The consequence is that if you want the optimal measurement at the origin you have to start the filter from the end of the track**

**After all the measurements have been used (filtered) it is possible possible to build a procedure that**

> **uses the (stored) intermediate results of the filter**

**gives the best parameter estimation at any point**

**This is the smoother**



**Applications of Kalman Filter:**

**navigation**

**radar tracking**

**sonar ranging**

**satellite orbit computation**

**stock prize prediction**

**It is used in all sort of fields**

**Eagle landed on the moon using KF**

**Gyroscopes in airplanes use KF**

**Usually the problem is to estimate a state of some sort and its uncertainty**

**location and velocity of airplane**

**track parameters of charged particles in HEP experiments**

**However we do not observe the state directly**

**We only observe some measurements from sensors which are noisy:**

**radar tracking**

**charged particle tracking detectors**

**As an additional complication the state evolve in time with is own uncertainties: process stochastic noise**

> **deviation from trajectory due to random wind**

**multiple scattering**

**In case of tracking in HEP instead of time we can consider the evolution of the track parameter at the discrete layers where the detectors perform the measurement**

**We give here the basics equations of the Kalman Filter**

**Detailed discussion can be found in [2: Bock et al 1990], [6: Avery 1992], [7: Frühwirth 1987], [8: Billoir 1985]**

#### **Consider 2 planes of our system**



**The measurements up to plane** *k* **- <sup>1</sup> allowed us to get an estimate of the track parameters <sup>p</sup>***k***-1**

We then propagate  $\bm{{\rm p}}_{k\text{-}1}$  to plane  $k$ 

$$
\tilde{\mathbf{p}}_k = \mathbf{F}_k \mathbf{p}_{k-1} \quad F_k = \frac{\partial \mathbf{f}_k}{\partial \mathbf{p}_{k-1}}
$$

 $\tilde{\textbf{p}}_k$ The covariance matrix  $\mathbf{C}_k$  of  $|\tilde{\mathbf{p}}_k|$ is

$$
\mathbf{C}_k \, = \, \mathbf{F}_k \mathbf{C}_{k-1} \mathbf{F}_k^{\mathbf{T}} \, + \, \mathbf{M}_{ms}
$$

The covariance matrix of  $p_{k-1}$  is  $C_{k-1}$ <br>
The covariance matrix  $C_k$  of  $\left[\tilde{p}_k\right]$  is<br>  $C_k = F_k C_{k-1} F_k^T + M_{ms}$ <br>
The matrix  $M_{ms}$  accounts for the et<br>
of multiple scattering on the parame<br>
covariance matrix<br>
On pl **The matrix M***ms* **accounts for the effect of multiple scattering on the parameters covariance matrix**

**On plane** *k* **we have some measurements**  $m_k$  with a covariance matrix  ${\bf V}$ 

**Using the track model (***k* **means: origin at plane** *k* **! )**

$$
\mathbf{y}_k = \mathbf{H}_k \mathbf{p}_k
$$

**track parameter at plane**  $k$ **:**  $\frac{\tilde{\textbf{q}}_k}{\tilde{\textbf{q}}_k}$ **we can obtain a second estimate of the** 

$$
\chi^2 = \left(\mathbf{y}_k - \mathbf{m}_k\right)^T \mathbf{V}^{-1} \left(\mathbf{y}_k - \mathbf{m}_k\right)
$$

$$
\chi^2 = \left(\mathbf{H}_k \mathbf{p}_k - \mathbf{m}_k\right)^T \mathbf{V}^{-1} \left(\mathbf{H}_k \mathbf{p}_k - \mathbf{m}_k\right)
$$

minimizing  $\chi^2$  gives the second estimate



#### **Summarising we have**

**the estimate propagated**

 $\mathbf{p}_k$ ~

**with its covariance matrix**

**The second estimate from the measurement at plane** *k*

 $\tilde{\textbf{q}}_k$ 

#### **with its covariance matrix**

**We can obtain a proper weigthed average of those 2 estimate**

**This is the filtered value at plane** *k*

**Details and formulas can be found in the cited references**

**The advantage of this method are**

**it is clearly iterative**

**at each step the problem has low dimensionality and no large matrix has to be inverted**

**the computation time increases only linearly with the number of detectors**

**The estimated track parameters closely follows the real path of the particle**

**the linear approximation of the track does not need to be valid over the whole track length but only from one detector to the next**

#### **Conclusions**

**We have seen the basic aspects of tracking with and without magnetic fields In both cases we have shown the use of powerful and easy linear models We have discussed optimization of momentum resulution: track length impact parameter resolution: vertex detector + central detector We have discussed the importance of multiple scattering at low momentum We have introduced the Kalman Filter a powerful iterative technique to optimally solve the tracking problem**

### **I Hope It Is Rather A Beginning**

**I hope you found tracking interesting and that soon some of you will work on the tracking detector of his/her experiment**

## **References**

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- **4 Avery P. Applied fitting teory I: General Least Squares Theory Cleo note CBX 91-72 (1991) see: http//www.phys.ufl.edu/~avery/fitting.html**
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- **7 Frühwirth R. Application of Kalman Filtering to Track and Vertex Fitting NIM A262 p. 444 (1987)**
- **8 Billoir P. Track Element Merging Strategy and Vertex Fitting in Complex Modular Detectors NIM A241 p. 115 (1985)**

**thank you for reading this lecture note: I hope you found it useful.**

**If you find errors I will be grateful if you send me an email at francesco.ragusa@mi.infn.it**